

MALEVANSKIY, V. D.; POZDNYAKOV, V. G.; POZDNYAKOV, V. G.; POZDNYAKOV, V. G.

Problems of the airtightness of the casing space manifold of gas
wells. Gaz. prom. 6 no.8, 16 '61. (MIRA 11-12)
(Gas wells)

YATROV, Sergey Nikolayevich; GOL'DSHTEYN, Izrail Yefremovich; GLUSECHENKO, Yekaterina Ivanovna; LATUKHINA, Ye.L., vedushchiy red.; POLOSINA, A.S., tekhn. red.

[Natural drilling fluids for drilling gas wells under complex conditions] Estestvennye promyvochnye zhidkosti dlia burenia gazovykh skvazhin v oslozhnennykh usloviakh. Moskva, Gos. nauchno-tekhn. izd-vo neft. i gorno-toplivnoi lit-ry, 1961. 41 p. (MIRA 14:7)
(Shebelinka region--Drilling fluids)

BRUNELL, C. and BRUNELL, M.A.; *Environ. Sci. Technol.*, 1977, 11, 103.

1. Vozneznitskiy Indebeneder der Gesellschaft der
Effekt (Kontingenz)

GOLUBOV, I.Z., 1941.

Gutter spout funnel warned by the air discharged from
premises. Vol.1 ser.1. no.4:18 Apr '45.

(PLA 19:1)

RUDIN, Naum Grigor'yevich; KUPRIN, A.V., retsenzent; GOL'DSHTEYN, Zh. A.
redaktor; MEDVEDEVA, L.A., tekhnicheskiiy redaktor

[Guide to a knowledge of color] Rukovodstvo po tsvetovedeniiu.
Moskva, Gos. nauchno-tekhn. izd-vo M-va legkoi promyshl. SSSR,
1956. 45 p. and 25 plates (in portfolio) (MLRA 10:5)

1. Chlen-korrespondent Akademii khudozhestv SSSR. (for Kuprin)
(Color)

73
KULIGIN, Aleksandr Vasil'yevich; GOL'DSHTEYN, Kh.A., redaktor; POPOVA, T.G.,
tekhnicheskiiy redaktor

[Jacquard looms; construction, repair and adjustment] Zhakkardovye
mashiny; ustroystvo remont i naladka. Moskva, Gos. nauchno-tekhn.
izd-vo Ministerstva legkoi promyshl. SSSR, 1956. 135 p. (MLRA 10:1)
(Jacquard weaving)

LUKASHEV, I.A.; PETROPOL'SKAYA, N., red.; GOL'DSHTEYN, L., red.;
ANTONOV, V., tekhn. red.

[A new irrigation system] Novaya sistema orosheniia.
Kuibyshev, Kuibyshevskoe obl.gos.izd-vo, 1953. 61 p.
(MIRA 16:8)

(Kuybyshev Province--Irrigation)

KAPITONOV, I.; STEPANOV, A., red.; GOL'DSHTEYN, L., red.; ANTONOV, V.,
tekhn.red.

[For high quality of production] Za vysokoe kachestvo produktsii.
Kuibyshevskoe knizhnoe izd-vo, 1953. 34 p. (MIRA 12:3)

1. Sekretar' tsekhovoy partiynoy organizatsii zavoda "Avtotrakto-
rodetal'" (for Kapitonov).
(Quality control)

22(1)

001/00-00-3-33/53

AUTHORS: Gol'dashteyn L.A. and Radchenko M.M., (Baku)

TITLE: Experience Working With Laboratory Radio Equipment

PERIODICAL: Fizika v shkole, 1979, Nr 3, pp 33-37 (USSR)

ABSTRACT: The authors describe the structural and methodological shortcomings of the laboratory radio equipment produced by the plants of Glavuchtekhprom and indicate means to overcome these shortcomings in practical training in secondary schools. The constructional shortcomings are: 1) feeding of the radio set by batteries of galvanic elements; 2) the filament resistor is very easily disintegrated. As shortcomings the authors list: 1) the use of pentodes type 2ZH2M or 2K2M, whereas the students study only triodes; 2) the fact that the feeding of a radio system by battery diverts teaching from life, as about 90% of the receivers produced by Soviet industry are fed by alternating current; 3) the sym-

Card 1/2

SN/47-59-3-33/53

Experience Working With Laboratory Radio Equipment

Bols intended to guide the assembly work are formed according to the visual appearance of the parts and make assembly too easy. The last shortcoming could be easily eliminated by taking the eight assembly diagrams from the description of the equipment. The other shortcomings were overcome by: 1) replacing battery feeding by alternating current (full-wave kenotron rectifier with filter and half-wave selenium rectifier with filter); 2) using six-volt tubes type 6K7 or 6Zh7. Moreover, in order to facilitate the assembly work by students, the authors recommend the use of triodes type 6CS instead of pentodes type 6K8L or 6Zh8L.

Cont 1/2

GOL'DSHTEYN, M.A. (Laku)

Utilizing an electronic oscillograph in experiments on
acoustics. Fiz. v shkole 21 (vol:55-56 Jan-Feb 61) (KIEP 14:9)
(Sound)

GOLUBSHIN, I.S., Inst.; LADNITSKIY, I.S., Koms. tekh. nauk

Defects in the working surface of roller chain of mechanism
with iron. U.S. pat. no. 3,454, 744.

(U.S. Pat. 3,454, 744)

GOL: DSHTEYN L.P.

Distributor: J. I. K. in London H. B. [Gol: DSHTEYN L.P.]
 D. I. Zernov, N. V. [Gol: DSHTEYN L.P.]
 "Sovetskoe Radio", Moscow, 1956. 635 p. 16.50 rubles.
 Textbook to be used in course for radio technicians.
 Contains a systematic presentation of the theory of the
 electromagnetic fields starting from elementary phenomena,
 including Maxwell's equations and emphasizing rapidly changing fields.

AUTHORS: Cherenkov, A.A., Al'tshuler, A.E., Ryzhkova, B.M.,
Gol'dshteyn, L.D., Shnayder, G.S., Osipov, L.N., and
Zhadanovskiy, N.B.

65-6-6/13

TITLE: Hydropurification of sulphurous petroleum products on an
industrial installation. (Gidroochistka sernistykh nefte-
produktov na promyshlennoy ustanovke).

PERIODICAL: "Khimiya i Tekhnologiya Topliva i Masel" (Chemistry and
Technology of Fuels and Lubricants) 1957, No.6, pp.36-41
(USSR).

ABSTRACT: It is expected that hydropurification of sulphurous pet-
roleum products will be widely used in the U.S.S.R. in the
near future. On the basis of data on the process obtained
by VNII NP and LEN NII, an industrial plant was designed
and built by Giproneftezavod on one of the refineries. The
plant is described (fig.1). The process is carried out
using alumo-cobalt-molybdenum catalyst (developed by VNII
NP) and hydrogen (99%), obtained by catalytic conversion
of hydrocarbon gases. Straight run distillates and second-
ary products are being treated to produce Diesel fuel
(GOST 4749-49). Plant operating conditions are given in
table 1 and the results of purification of straight run
distillate from a mixture of Mukhanovskoy, Tuymazinskoy-
Devonskoy and Bavlinskoy crude oils, light gas oil from

Card 1/3

Hydropurification of sulphurous petroleum products on an industrial installation. (Cont.)

65-6-6/13

catalytic cracking (from 200-500° fraction) and a 1:1 mixture of the above two distillates in table 2. The degree of desulphurisation 95.2-95.8%. The analysis of gases obtained during hydropurification is given in table 3. The circulating gas before the absorber (with monoethanolamine) contained 0.7-0.9 volume % of hydrogen sulphide, after the absorber - 0.1%. The mean balance of the products of hydropurification is given in table 4. Hydrogen consumption for straight run distillate was 0.38 wt % and for gas oil from catalytic cracking - 0.71 wt %. Hydrogen used for the reaction was 0.27% and 0.60% respectively. The sulphur balance is given in table 5. Up to 0.03% of H₂S calculated on the raw material used is carried out with treated fuel and is removed by washing with 2.5 - 4% NaOH solution. The alkali consumption 0.1 kg per ton of Diesel fuel. The working period of the catalyst without regeneration is 8000 hrs. The regeneration of the catalyst is carried out at a temperature not exceeding 550° under 40 atm. pressure with a mixture of an inert gas with air. Initial oxygen concentration 0.2 - 0.25 vol % and at the end of the regenerating period is increased to 1.4%. When the main

Card 2/3

Hydropurification of sulphurous petroleum products on an industrial installation. (Cont.)

65-6-6/13

part of the "coke" was burned out, the remaining part was removed by increasing oxygen concentration to 2% and pre-heating the gas to 520-550 C (2 hours). Total duration of the regeneration process 20 hours. The initial activity of the catalyst is completely restored. When the plant was stopped for inspection it was found that the upper layer of the catalyst was covered with iron sulphide. Accumulations of iron sulphide were found in various places, i.e., the corrosion of the apparatus was noticeable. The parts of the apparatus containing H_2S and H_2 at high temperatures were made from steel X5M, the remaining part from mild steel. Apparently the corrosion resistance of X5M steel was insufficient. The precipitation of iron sulphide on the catalyst has no apparent influence on its activity. There are 5 tables and 1 figure.

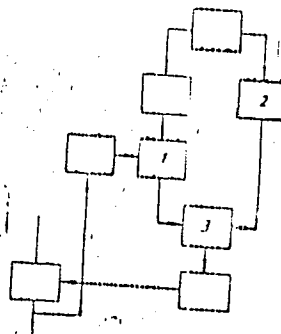
ASSOCIATION: VNII NP; Orgneft).

AVAILABLE:

Card 3/3

ACC NR: AP6015629

Fig. 1. 1 - periodically triggered parametric oscillator; 2 - autonomous parametric oscillator; 3 - discrete comparison circuit



of the reference parametric oscillator and the phase-sensitive parametric oscillator. Orig. art. has: 1 figure.

SUB CODE: 09/ SUBM DATE: 12Jun65

Card 2/2

SIVERS, Arkadiy Petrovich; SUSLOV, Nikolay Aleksandrovich; MMEPEL'SKIY,
Vasiliy Ignat'yevich; GOL'DSHTEYN, I.D., nauchnyy red.;
SHAURAK, Ye.N., red.; ERASTOVA, N.V., tekhn.red.

[Principles of radar] Osnovy radiolokatsii. Leningrad, Gos.
soiuznoe izd-vo sudostroitel'.promyshl., 1959. 350 p.

(Radar)

(MIRA 12:8)

SHATS, Solomon Yakovlevich; SUBASHIYEV, V.K., retsenzent; GOL'DSHTEYN,
L.D., retsenzent; VLAGOVA, Z.V., red.; KOROVENKO, Yu.N.,
tekhn. red.

[Transistors and principles of their operation] Tranzistory i
osnovy ikh primeneniia. Leningrad, Sudpromgiz, 1960. 135 p.
(MIRA 15:5)

(Transistors)

..AROV, Veniamin Israilevich; GOLDSHEIN, L.D., retsennant; VILNITSKY,
B.I. retsennant; ROZAL, H.L., nauchnyy red.; LITVIN, B.I.,
red.; ISAL, H.K., tekhn. red.

[Radar display units]Indikatornye ustroistva s avtomaticheskimi
nykh stantsii. Leningrad, Sudpromgiz, 1962. 431 p.

(Radar)

(RADA 13:10)

SHATS, Solomon Yakovlevich; PEROV, G.I., kand. tekhn. nauk,
retsenzent; GOL'DSHTEYN, L.D., nauchnyy red.; SACHUK,
N.A., red.; KOROVENKO, Yu.N., tekhn. red.

[Transistors in pulse techniques] Tranzistory v impul'-
snoi tekhnike. Leningrad, Sudpromgiz, 1963. 250 p.

(MIRA 15:7)

(Transistors) (Pulse techniques (Electronics))

AUTHORS:

Osipov, A.I., Shvartsman, V.A., Alekseyev, V.I., Gurev, V.I.
Kashin, A., Pulyaev, A., Gurev, A.I., Gurev, A.I., Gurev, A.I.
Gurev, A.I., Gurev, A.I., Gurev, A.I., Gurev, A.I., Gurev, A.I.

09-11-22/3

TITLE:

The Use of Radio Isotopes when Investigating the Kinetics of Scrap
Fusion and Slag Formation in the Smelting of Iron. (Russian)
The article describes the results of the investigation of the kinetics of
slag formation and the fusion of scrap in the smelting of iron.

IDENTIFIERS:

Aluminum, Scrap, Iron, Steel, Smelting, Slag. (Russian)

ABSTRACT:

1) Kinetics of the fusion of scrap. The fusion velocity in the iron and steel scrap is shown on the basis of the calculation of the specific activity of standard metal samples (G-60), which contain G-60 with the help of measuring tubes of the G-60 type. From the dependence obtained between the metal scrap quantity and the time which an weighed scrap introduction of the scrap, it follows that nearly half of the scrap is melted already after about 200 minutes.

2) Investigation of the kinetics of slag formation. On the basis of the results of the investigation, it was found that the slag is formed in the liquid slag in closed measuring tubes and standard samples for measuring are taken out only after a lapse of time of 2-3 minutes. An experiment was made to determine the time in which the slag dissolves in the slag, the reaction.

Card 1/2

The Use of Small Tracers When Investigating the Kinetics of Urea. 11-11-24/36
Fusion and Gaseous Reaction in the Carapace Process.

$\frac{dx}{dt} = k_1(1-x) - k_2x$ was experimentally verified.

x here denotes the weight of the already dissolved urea and k_1 the proportionality coefficient for a 25% reaction. There are 2 figures and 3 table references.

SUBMITTED
AVAILABLE

January 12, 1937
Library of Congress

Card 2/2

SOV/137-68-9-1896b

Translation from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 9, p. 1, 6 (USSR)

AUTHORS: Gorenshcheyn, M.M., Goldshcheyn, L.G.

TITLE: A Nucleonic Method of Investigating Pick-up of Metal on the
Rolls of a Blooming Mill (Metod issledovaniya nalipaniya
metalla na valki blyuminga s primeneniym radioaktivnykh
izotopov)

PERIODICAL: Sb. nauchn. tr. Zhdanovsk. metallurg. in-t, 1957, Nr 4,
pp 153-156

ABSTRACT: The pickup of metal by the rolls of a blooming mill in the
process of rolling is investigated by means of isotopes at the
blooming mill of the Stalino Metallurgical Plant. Radioactive
 P^{32} was introduced into the ladle with the molten metal. Ingots
made from this metal were rolled on the blooming mill. After
rolling, the rolls were removed and turned on lathes. The
chip was collected and its radioactivity recorded. The differ-
ence between the radioactivity of the chip samples and the back-
ground testified to pick-up of metal from the ingot by the bloom-
ing-mill rolls. The work performed does not yet permit the
drawing of any quantitative conclusions.

Card 1/1

A. F.
1. Rolling mills--Performance. 2. Metal--Pickup. 3. Isotopes--Applications.
4. Radioisotopes--Applications.

137-58-4-6740

Translation from Referativnyy zhurnal Metallurgiya 1958, Nr 4, p 63 (USSR)

AUTHORS Gerchikov, D.S., Goldshteyn, L.G., Otengender, A.M.

TITLE A Radioactive-isotope Investigation of the Nature of Accumulations of Non-metallic Inclusions in Rimmed Steel (Issledovaniye prirody skopleniy nemetallicheskiykh vklyucheniyy v kapyashchey stali s pomoshchyu radioaktivnykh izotopov)

PERIODICAL Tr. Donetsk. otd. Nauchno-tekhn. osv. chernoy metallurgii 1957, Nr 5, pp 102-123

ABSTRACT The investigation was performed with the aid of the radioactive isotope (RI) Ca^{45} , 0.83-17.26 millicurie being added per ton of steel to steel rimming in the mold. The addition was in the form of a mixture of Ca^{45}O and slag. The isotope was also used in the runner brick by impregnating it with a solution containing Ca^{45}O . Determination of radioactivity by the "thick layer" method was made in samples of slag removed from the surface of the steel in the molds, and in nonmetallic inclusions (NI) precipitated from specimens of the metal when rolled. It was established that when the RI was introduced into the slag the unit radioactivity of the NI varied from 29 to 3658 impulses

Cord 1-2

137-58-1-1-040

A Radioactive-isotope investigation (cont.)

per minute, or in the range of 0.63 to 36.5% of the radioactivity of the slag. The samples containing RI in NI came from all levels of the ingot, and the number of samples with RI ranged from 41.2 to 83.5% of those taken from the height, and from 57.3 to 65% of those taken across the section of the ingot. It is remarked that the largest number of specimens having a high RI content was found in the center of the ingot, and the largest amount of RI in the specimens was found at $\leq 9\%$ from the top of the ingot. When RI was introduced into bulk refractory for runners, specimens containing RI were also found at all levels in the ingot, but the maximum amount of RI was found in specimens from the edge of the ingot and at distances of 10% and more from its top. It is noted that contamination of runned steel by NI due to construction of runner brick is of random nature, and that diminution of the NI formed by entry of slag from the surface of the riser into the ingot makes for diminution of running of the metal in the mold and for mechanical separation of slag therefrom. Measures are recommended to reduce rejects of steel due to accumulations of NI, namely, pouring at 1600-1620° Fe-Mn deoxidation in the ladle and use of flux mixtures consisting of 65% sand and 35% scale to liquify the slag in the mold. Bibliography: 18 references.

A 5L

Card 2/2

18(0) PHASE I BOOK EXPLOITATION SCV/2135
Teatral'nyy nauchno-issledovatel'skiy Institut Chernoy Metallurgii.
Institut Metallovedeniya i fiziki metalliv
Problemy metallovedeniya i fiziki metalliv (Problemy v fizikal'noy metallografii i metallofizike) Seriya: Metallovedeniye, 1959, 3,600 copies printed.
Additional Sponsoring Agency: USSR, Gosudarstvennaya planovaya komissiya
Ed. of Publishing House: Ye. M. Berlin; Tech. Ed.: P. G. Zolotarev; Editorial Board: D. S. Kamenets, Ye. M. Lyskov (Resp. Ed.), Ye. L. Spector, L. M. Utevisky, L. A. Shvartsman, and V. I. Malkin.
PURPOSE: This book is intended for metallurgists, metallurgical engineers, and specialists in the physics of metals.
COVERAGE: The papers in this collection present the results of investigations conducted between 1954 and 1958. Subjects covered include crystallization of metals, physical methods of investigating the processes of crystallization, physical metallurgy of metallurgical production, problems in the new methods and equipment for investigating steels, and production control. References follow each article.

TABLE OF CONTENTS:

PART I. CRYSTALLIZATION OF METALS

- 318
319
320
321
322
323
324
325
326
327
328
329
330
331
332
333
334
335
336
337
338
339
340
341
342
343
344
345
346
347
348
349
350
351
352
353
354
355
356
357
358
359
360
361
362
363
364
365
366
367
368
369
370
371
372
373
374
375
376
377
378
379
380
381
382
383
384
385
386
387
388
389
390
391
392
393
394
395
396
397
398
399
400
401
402
403
404
405
406
407
408
409
410
411
412
413
414
415
416
417
418
419
420
421
422
423
424
425
426
427
428
429
430
431
432
433
434
435
436
437
438
439
440
441
442
443
444
445
446
447
448
449
450
451
452
453
454
455
456
457
458
459
460
461
462
463
464
465
466
467
468
469
470
471
472
473
474
475
476
477
478
479
480
481
482
483
484
485
486
487
488
489
490
491
492
493
494
495
496
497
498
499
500
501
502
503
504
505
506
507
508
509
510
511
512
513
514
515
516
517
518
519
520
521
522
523
524
525
526
527
528
529
530
531
532
533
534
535
536
537
538
539
540
541
542
543
544
545
546
547
548
549
550
551
552
553
554
555
556
557
558
559
560
561
562
563
564
565
566
567
568
569
570
571
572
573
574
575
576
577
578
579
580
581
582
583
584
585
586
587
588
589
590
591
592
593
594
595
596
597
598
599
600
601
602
603
604
605
606
607
608
609
610
611
612
613
614
615
616
617
618
619
620
621
622
623
624
625
626
627
628
629
630
631
632
633
634
635
636
637
638
639
640
641
642
643
644
645
646
647
648
649
650
651
652
653
654
655
656
657
658
659
660
661
662
663
664
665
666
667
668
669
670
671
672
673
674
675
676
677
678
679
680
681
682
683
684
685
686
687
688
689
690
691
692
693
694
695
696
697
698
699
700
701
702
703
704
705
706
707
708
709
710
711
712
713
714
715
716
717
718
719
720
721
722
723
724
725
726
727
728
729
730
731
732
733
734
735
736
737
738
739
740
741
742
743
744
745
746
747
748
749
750
751
752
753
754
755
756
757
758
759
760
761
762
763
764
765
766
767
768
769
770
771
772
773
774
775
776
777
778
779
780
781
782
783
784
785
786
787
788
789
790
791
792
793
794
795
796
797
798
799
800
801
802
803
804
805
806
807
808
809
810
811
812
813
814
815
816
817
818
819
820
821
822
823
824
825
826
827
828
829
830
831
832
833
834
835
836
837
838
839
840
841
842
843
844
845
846
847
848
849
850
851
852
853
854
855
856
857
858
859
860
861
862
863
864
865
866
867
868
869
870
871
872
873
874
875
876
877
878
879
880
881
882
883
884
885
886
887
888
889
890
891
892
893
894
895
896
897
898
899
900
901
902
903
904
905
906
907
908
909
910
911
912
913
914
915
916
917
918
919
920
921
922
923
924
925
926
927
928
929
930
931
932
933
934
935
936
937
938
939
940
941
942
943
944
945
946
947
948
949
950
951
952
953
954
955
956
957
958
959
960
961
962
963
964
965
966
967
968
969
970
971
972
973
974
975
976
977
978
979
980
981
982
983
984
985
986
987
988
989
990
991
992
993
994
995
996
997
998
999
1000

GOLDSHTEYN, L. M.

DECEASED

1963/1

c. 1962

MEDICINE
(Cancer)

see ILC

1 06130-61 MAP(a)/MAP(a)/MAP(a)/MAP(a) DE
ACC NR: AP6026707

SOURCE CODE: UR/0181/66/008/008/2467/2469

AUTHOR: Adirovich, E. I.; Gol'dshteyn, L. M.

ORG: Physicotechnical Institute, AN UzSSR, Tashkent (Fiziko-tekhnicheskiy institut AN UzSSR)

TITLE: Determination of the forbidden gap width of single-crystal boron by the "intrinsic thermometer" method

SOURCE: Fizika tverdogo tela, v. 8, no. 8, 1966, 2467-2469

TOPIC TAGS: forbidden zone width, boron

ABSTRACT: The "intrinsic thermometer" method, described earlier by the authors (DAN SSSR, 153, 313, 1964) and used for measuring and continuously checking the temperature of a current-carrying silicon wafer serving as the evaporator in the vacuum deposition of silicon films, was applied to the study of single-crystal boron. Measurements over a wide temperature range, up to the melting point of boron (2573°K), were performed by recording the volt-ampere characteristics of crystals heated by the current passing through them. From the values of V and I obtained, the values of ρ were calculated and plotted against the temperature. The resulting function $\rho(V)$ can be used to characterize the temperature of the crystal at a given V , since in the region of intrinsic conductivity the resistivity of the semiconductor is a single-valued function of temperature. The conversion to the absolute temperature scale was made by using the

Card 1/2

L 06430-5"

ACC NR: AP6026707

formula

$$\rho = \rho_0 \exp \left[T_1 \left(\frac{1}{T} - \frac{1}{T_0} \right) \right], \quad (1)$$

The values of T_1 , ρ_0 and E_g for boron, determined by the "intrinsic thermometer" method, were found to be: $T_1 = 6750^\circ\text{K}$; $\rho_0 = 10^7 \text{ ohm cm}$; $E_g = 2kT_1 = 1.16 \text{ eV}$. Orig. art. has: 2 figures and 2 formulas.

SUB CODE: 20/ SUBM DATE: 29Jan66/ ORIG REF: 004/ OTH REF: 004

Card 2/2 *llh*

D 14380-65 EWT(1)/EWT(m)/T/EWP(t)/ESQ(b)-2/EWP(b) IJP(t)/ASD(a)-5/
AFWL/ESD(dp)/ESD(t) JD/GG
ACCESSION NR: AP4045626 S/0020/64/158/002/0313/0316

AUTHOR: Adirovich, E. I. (Academician AN U.S.S.R.); Goldshteyn, L. M.

TITLE: Films with anomalously large photovoltage, obtained by sublimation of Si atoms from the surface of a current-carrying silicon slab

SOURCE: AN SSSR. Doklady*, v. 158, no. 2, 1964, 313-316

TOPIC TAGS: thin film, silicon photocell, photoelectric current, sublimated film, anomalous photoemf

ABSTRACT: A procedure is proposed for obtaining thin films of silicon which develop anomalously large photoemfs when illuminated, and which were obtained first by H. Kallman, et al. (J. Electrochem. Soc. v. 108, 3, 247, 1961) and by E. I. Adirovich and Yu. M. Tshabov (DAN, 155, no. 6, 1964). The configuration and dimensions of the source in the described procedure create different conditions for the formation of the films during the course of sputtering. The evaporators used were silicon slabs (30 x 3 x 9.5 mm) cut from a p-type single

Card 1/3

L 14380-65

ACCESSION NR: AP4045626

crystal with 1 ohm-cm resistivity. The sputtering on the substrates was effected by passing current through the silicon slab and by sublimation of the silicon on the substrate. The methods used to regulate the temperature of the evaporator and of the substrates are described. The procedure is similar to that used by Kolgorov and Roberts (Review Scientific Instruments, v. 34, no. 1, 11, 1963) to deposit chemically active semiconductor surfaces. Data are presented on 10 out of 50 films produced. The films produced have properties similar to those described by the author elsewhere. "The authors are grateful to G. A. Kurov and L. A. Zhukova for electron diffraction studies of the films, and also to O. G. Bakradze for participating in the experiments. Orig. art. has: 2 figures, 3 formulas, and 1 table.

ASSOCIATION: Fiziko-tekhnicheskiy institut Akademii nauk UzSSR
(Physicotechnical Institute, Academy of Sciences, UzSSR)

SUBMITTED: 07May64

ENCL: 01

SUB CODE: SS, OP.

NO IFF SOV: 004

OTHER: 007

Card 2/3

L 14380-65
ACCESSION NR: AP4045626

ENCLOSURE: 01
0

№	R_{ohm}	d, μ	V_{alp}	$T_{\text{eff}}^{\circ}\text{C}$	$T_{\text{sub}}^{\circ}\text{C}$
1	$5 \cdot 10^{12}$	1,25	38	1170	168
2	$2 \cdot 10^{12}$	3,02	21	1170	150
3	$7 \cdot 10^{12}$	1,42	35	1170	230
4	$1 \cdot 10^{12}$	2,3	42	1240	145
5	$1,5 \cdot 10^{12}$	1,16	70	1240	78
6	$1,8 \cdot 10^{12}$	2,84	40	1270	211
7	$2 \cdot 10^{12}$	1,37	30	1270	195
8	$1 \cdot 10^{12}$	0,98	72	1320	242
9	$2,7 \cdot 10^{12}$	1,43	54	1320	242
10	$4 \cdot 10^{12}$	1,54	36	1320	90

Fig. 1. Results of measurements

R - Resistance, ohms; d - film thickness, microns; V_{alp} - anomalously large photovoltage, V; T_{eff} - temperature of silicon slab; T_{sub} - substrate temperature.

Card 3/3

GOL'DSTEYN, L. V.

Mathematical Reviews
Vol. 14 No. 7
July - August 1953
Geometry

Gol'dstejn, L. V. Construction of a projective theory of curves by means of central affine geometry. Trudy Sem. Vektor. Tenzor. Analizu 9, 238-308 (1952). (Russian)

In the present paper the curve theory in a two- or three-dimensional projective space is reconstructed, i.e., the projective length $\sigma = \int p^{1/2} du$ defined by the integral invariant p of the lowest order and the projective curvatures of a curve are calculated from the standpoint of central-affine geometry, as usual, making use of absolute differentiation in a one-dimensional space and of projective normalization of point coordinates. It is also verified that $p=0$ characterizes a conic in a projective plane or a curve belonging to a linear complex in a projective space; and then the Frenet formulas are obtained. The method used is not different from the usual one and the reviewer could not find original concepts or new results. The author seems to be not familiar with the book by G. Fubini and E. Cech [Geometria proiettiva differenziale, t. I, Zanichelli, Bologna, 1926].

Kawaguchi (Sapporo).

GOL'DSHTEYN, Leonid Vladimirovich, inzh.; TABUNINA, M.A., red. izd-
va; TARKHOVA, K.Ye., tekhn. red.

[Safety manual for electricians servicing construction
equipment] Pamiatka po tekhnike bezopasnosti dlia elektro-
montera po obsluzhivaniyu stroitel'nykh mekhanizmov. Izd.2.,
perer. i dop. Moskva, Gosstroizdat, 1963. 81 p.

(MIRA 16:9)

(Construction equipment--Safety measures)

GOL'DSHTEYN, L.Ye.

U S S R

The constitution of structuralis martensite (barkentia).
A. S. Zay'ev and L. Ye. Gol'dsh'teyn. Zhur. Tekh. Fiz.
23, 817-20 (1953).—It was found that structuralis martensite
site does not have an regular structure. G. S. Macj

GOL'DSHTEYN, L. Ya.

Structure of reversible superconductors. The samples were prepared by the method of Chatterjee et al. [6]. Specimens of iron-based Nb_{0.8}Sr_{0.2}C_{0.97}Ta_{0.03}C_{0.5}Ni_{0.5}, U_{0.8}C_{0.2} and Nb_{0.8}Sr_{0.2}C_{0.97}Ta_{0.03}C_{0.5}Ni_{0.5} were annealed from 1150° down to 200° at 500° and then either water-quenched or furnace-cooled. Electron micrographs of polished specimens showed that the grain boundaries were wider in the furnace-cooled specimens. Electron micrographs of the fracture surfaces revealed plastic deformation in the furnace-cooled specimens but not in the water-quenched specimens. Electron diffraction patterns of carbides isolated from fractured surfaces having a brittle fracture showed normal cementite lines, while the patterns from ductile or shear fracture showed distorted cementite. This difference was attributed to coherency of the cementite with the matrix in the ductile case.

Central Sci Res Inst, Ministry of Construction Industry,

THE

137-58-4-8147

Translation from Referativnyy zhurnal, Metallurgiya, 1958, Nr 4, p 255 (USSR)

AUTHORS: Zav'yalov, A.S., Goldshteyn, L.Ya., Senchenko M.I.

TITLE The Nature of Temper (Heat) Brittleness [O prirode otpusknoy (teplovoy) khrupkosti]

PERIODICAL: V sb.: Metallovedeniye, Leningrad, Sudpromgiz, 1957, pp 127-144

ABSTRACT: As a supplement to the hypothesis of one of the authors (Zav'yalov, "On the Theory of the Alloying and the Heat Treatment of Steel," TsNII NKTP, 1943) to the effect that temper brittleness (TB) is induced by the appearance of particles of precipitated phases on the boundaries of what had previously been austenite grains it is postulated that the enrichment of such surfaces in the tempering process by certain elements dissolved in Fe increases the σ_s and diminishes the resistance of these zones to fracture, and this leads to the appearance of TB. This explains the high temperature of TB of high-phosphorus steels, while the absence of carbide particles (K) along the boundaries of the former austenite grains is explained by the mutual dislodging of P and C. In TB due to K precipitation, TB

Card 1/2

137-58-4-8147

The Nature of Temper (Heat) Brittleness

maximums are observed after low-temperature tempering over specific extended periods of time. This is occasioned by the simultaneous processes of precipitation of new particles of K due to the C supersaturating the ferrite and to the dissolution of fine precipitates within the grain and the fact that they come down on the boundaries, which increases the TB, and the processes of K coagulation along the grain boundaries, which decreases it. The mechanism of K redistribution is confirmed by the electron microscope and the electron diffraction camera. Reduction in TB when the duration of pre-tempering over 600° is increased is explained by reduction in the supersaturation of the ferrite by C, coagulation of small K, and enrichment thereof by alloying elements, thereby increasing their resistance to dissolution. See also RzhMet. 1957, Nr 10, abstract 20085.

1 Steel--Brittleness--Analysis of Steel--Mechanical properties--Effects of heat treatment A K

Card 2/2

AUTHOR: Zav'yalov, A.S., Doctor of Technical Sciences, Prof.,
Gol'dshteyn, L.Ya., Engineer, and Senchenko, M.I.,
Engineer. 129-4-5/17

TITLE: On the problem of temper (thermal) brittleness. (O
prirode otpusknoy (teplovoy) khrupkosti).

PERIODICAL: "Metallovedenie i Obrabotka Metallov" (Metallurgy and
Metal Treatment) 1957, No. 4, pp. 21 - 30 (U.S.S.R.).

ABSTRACT: On the basis of tests carried out the authors estab-
lished that the temper (thermal) brittleness is due to
enrichment of the boundary zones of what were previously
austenite grains by various admixtures; some of the ad-
mixtures in the boundary zones are present in the form
of isolated phases as, for instance, carbon in the form
of carbides, whilst others are present in the dissolved
state (for instance, P, however, in the case of high P
contents phosphides may form). During enrichment of the
boundary zones by admixtures a decrease of the breaking
strength of these zones will occur which in many cases is
accompanied by an increase of the yield point. As a
result of this there will be an increase in the critical
temperature of the brittleness of these zones which will
bring about brittle fracture of the metal along the bound-
ary zones. If the brittle fracture is not along the

Card 1/4

On the problem of temper (thermal) brittleness. (Cont.)

129-4-5/17

factors which bring about a uniform distribution of the admixtures throughout the grain reduce the brittleness of the steel and the tendency of the steel to develop brittle fractures along the grain boundaries. These conclusions are based on earlier work of the authors (5, 6, 9, 10), on literary data and on experiments which are described in this paper. In these, the behaviour of two melts of Cr-Mo steel with various P contents were investigated, the compositions of which were as follows: 0.40% C, 0.28% Si, 0.42% Mn, 0.031% S, 0.028% P, 3.03% Cr and 0.46% Mo; 0.39% C, 0.24% Si, 0.49% Mn, 0.031% S, 0.097% P, 2.87% Cr and 0.41% Mo. The following heat treatment regimes were applied: heating to $A_{c3} + 40^{\circ}\text{C}$, quenching in oil, tempering at 650°C for ten hours followed by quenching in water; same heat treatment with the difference that after tempering the specimens were cooled to 300°C in the furnace with a speed of 20°C/hr . The results of impact tests are plotted in Fig. 3, p. 24 and these show that the P content has a very pronounced influence on the tendency of the steel to develop temper brittleness. Electron microscopic investigations enabled to establish interesting features of the distribution of carbides in high P content steels after hardening and high temperature tempering. It

Card 3/4

GOLDSHTEYN, L. Y.

18(7)

PHASE I BOOK EXPLOITATION

SOV/1938

Metallovedeniye; sbornik statey, [vyp.] 2 (Study of Metals; Collection of Articles, [Nr] 2) [Leningrad] Sudpromgiz, 1958. 265 p. 4,000 copies printed.

Resp. Ed.: G.I. Kapyrin, Candidate of Technical Sciences; Ed.: Ye. A. Krugova;
Tech. Ed.: K.M. Volchok.

PURPOSE: This book is intended for metallurgists and metallurgical engineers.

COVERAGE: This is the second volume of collected scientific papers dealing with various problems in physical metallurgy, particularly in mechanical metallurgy and metallography. Topics covered include hydrogen embrittlement, intra-granular distribution of elements in alloys, effect of tempering on carbon redistribution, use of tritium to investigate certain phenomena in metals, effect of certain alloying elements on temper brittleness and hardenability of steel, strength of notched specimens of brittle steel, effect of strain hardening on the properties of an aluminum alloy, etc. The articles are concerned mainly with various types of steel, though some deal with nonferrous alloys.

Card 1/23

Study of Metals (Cont.)

SOV/1838

Gol'dshteyn, L. Ya., Engineer; A.S. Zav'yalov, Doctor of Technical Sciences, Professor; and P.A. Stoyanov, Candidate of Technical Sciences. Characteristics of the Fine Structure of the Intergranular Zones of Structural Steel Affected by Temper Brittleness

53

Authors' conclusions: (1) Electron diffraction study appears to be an effective means of revealing the difference in the crystal structure of carbides situated on the fracture surface of brittle and tough steel. (2) Carbides situated on the grain boundaries of brittle steel have a structure made up of relatively perfect crystals. (3) This type of structure confirms an idea previously expressed by A.S. Zav'yalov, L.Ya. Gol'dshteyn, M.I. Senchenko, and Ye. Ya. Paley [apparently in No. 1 of the present series] concerning the three stages of carbide formation. A basic point of this idea is that the second stage is concluded by the separation of carbides, i.e., the appearance of a boundary between the carbide particles and the phase in which they originated, and, hence, by the loss of cohesive bonds between them - - a phenomenon especially noticeable around the boundaries of former austenite grains. This, together with changes in concentration and

Card 5/23

GOLDSTEIN, L. Ya

25(1)

PHASE I BOOK EXPLOITATION

SOV/1553

Moscow. Dom nauchno-tekhnicheskoy propagandy im. F.E. Dzerzhinskogo

Sovremennyye splavy i ikh termicheskaya obrabotka (Contemporary Alloys and Their Heat Treatment) Moscow, Mashgiz, 1958. 329 p. 12,000 copies printed.

Additional Sponsoring Agency: Obshchestvo po rasprostraneniya politicheskikh i nauchnykh znaniy RSFSR.

Ed. (Title page): Yu. A. Geller, Doctor of Technical Sciences; Ed. (Inside book): V.V. Rzhavinskiy, Engineer; Tech. Ed.: B.I. Model'; Managing Ed. for Literature on Metal Working and Tool Making; R.D. Beyzel'man, Engineer.

PURPOSE: The book is intended for engineering and technical personnel of heat-treatment shops and test laboratories of machine-building plants.

COVERAGE: This collection of 28 articles, compiled by 33 authors, aims to acquaint the reader with modern practice in the heat treatment of steels. The authors

Card 1/6

Contemporary Alloys and Their Heat Treatment

SOV/1558

are primarily concerned with the development of various types of structural, tool, and heat-resistant steels and with the use of their alloying elements. Materials-handling equipment is described at some length. The treatment of alloys, particularly those of titanium, also comes within the scope of the collection. The book is thoroughly diagrammed, and a good deal of the material is shown in graphical form. Among the problems dealt with are the minimization of deformations, the introduction of the automatic control of heat-treating equipment, together with fully mechanized tool manufacture, and the optimum proportions of different alloying elements. There are numerous tables and drawings. Bibliographic listings placed at the end of chapters are predominantly Soviet. The articles comprising this collection are reports delivered at a conference held in the Scientific and Technical Propaganda House imeni F.E. Dzerzhinskiy in Moscow.

TABLE OF CONTENTS:

Foreword

3

Card 2/6

Contemporary Alloys and Their Heat Treatment

SOV/1558

Zav'yalov, A.S., L. Ya. Gol'dshteyn, and M.I. Senchenko. Nature of Temper Brittleness	5
Pogodin-Alekseyev, G.I., and M.M. Fetisova. Influence of Chemical Composition, Original Structure, and Test Conditions on the Temper Brittleness of Steel	23
Skotnikov, V.V. Intermediate Transformation of Austenite	40
Pogodina-Alekseyeva, K.M. Effect of Ultrasonic Waves on Transformations in Metals in the Solid State	48
Kontorovich, I. Ye. Principles of Alloying and New Types of Structural Steel	62
Meshcherinova, O.N. Structural Steels Alloyed with Boron	74
Tarasov, A.M. Study of Optimum Composition and of Some Peculiarities of the Heat Treatment of Boron-alloyed Case-hardened Structural Steel	80

Card 3/6

Contemporary Alloys and Their Heat Treatment	SOV/1558	
Perel'man, Ye. G. Proper Selection of Steels for Case-hardened Parts		93
Chirakov, V.T. Initial Data for Selecting Regimes for the Carburizing and Heat Treatment of Case-hardened Parts		104
Kel'min, A.T. A Modern Carburizing Agent for Gas Carburizing and Cyaniding		116
Rakhshtadt, A.G., O.N. Meshcherinova, and V.V. Zikiyev. Properties and Heat Treatment of Boron-alloyed Spring Steels		132
Geller, Yu. A. Improvements in the Composition and Heat Treatment of Tool Steels		149
Volkov, A.M. An Investigation of El603 Low-Alloy Steel as a Material for Cutting Tools		171
Ivanov, A.G. New Types of High-speed Steel		175
Golovin, G.F. Hardening and Tempering of High-speed Steels With Induction Heating		178
Card 4/6		

Contemporary Alloys and Their Heat Treatment	SOV/1558
Koroley, G.G.. Heat-treatment of Cutting Tools in an Atmosphere of Steam	186
Kayushnikov, P. Ya. Deformation of Steel in Quenching and Means of Preventing It	194
Nakhimov, D.M. Deformation of Steel in Heat Treatment	207
Khimushin, F.F. Heat-resistant Steels and Alloys Employed in the Construction of Gas Turbines	216
Vorob'yev, V.G. Changes in the Surface Layer of a Heat-resistant Alloy During Machining and Heating in an Oxidizing Medium	242
Shmykov, A.A. Rational Method of Obtaining Controlled Atmospheres From Gaseous Hydrocarbons	254
Assonov, A.D. Modern Automated Heat Treating Equipment	265
Card 5/ 6	

Contemporary Alloys and Their Heat Treatment	SCV/1558	
Shchelyakovskiy, K.Z. Future Prospects for the Use of High-Frequency Currents in Machine Building		279
Redotenko, N.S. Mechanization of the Heat Treatment of Tools		292
Pomerants, D.M. Magnetic Quality-control Method in the Heat Treatment of Parts		304
Iordanskiy, V.N. Weldable Aluminum-Magnesium Alloys		308
Tsyvkina, Ye. D. Fatigue Strength of Industrial Titanium		314
El'yasheva, M.A. Strength of Welded Joints Made of VT1D Industrial Titanium		319
AVAILABLE: Library of Congress		

GO/ksv
5-21-59

Card 6/6

GOL'DSHEYN, L.Ya., inzh.; ZAV'YALOV, A.S., prof., doktor tekhn.nauk;
STOYANOV, P.A., kand.tekhn.nauk

Characteristics of the fine structure of intercrystallite zones
in the state of temper brittleness. Metallovedenie 2:53-64 '58.
(MIRA 13:9)
(Steel, Structural--Metallography) (Crystal lattices)

AUTHORS: Fedin, M. Ya. and Gol'dshteyn, I. Ya. 3.7/126-4-1-32/72

TITLE: X-ray Microbeam Studies of Unformed Steels. I
(Izucheniye mikrobimovymi puchkami rentgenovskikh izlucheniy neodformirovannogo i neodformirovannogo sverkhprochnogo. I)

PERIODICAL: Fizika metallov i metallovedeniye, 1982, Vol. 5, No. 2, pp. 512-517 (USSR)

ABSTRACT: A special source tube with a focal spot diameter of 0.15 mm and a beam current of 1 mA. The beam is shaped to a 0.15 mm diameter circular spot of 40 μm diameter (or larger) in the object; back-reflection actions are used. Fig. 1 shows certain details of the deep-etching process; the film also includes other details. It gives the best results. Fe and Co are detected; a surface covered by the beam with a 0.15 mm diameter (70 μm) is etched by dropping 0.1 M HCl solution with the steel sample. A high-purity steel type 35 is used, normally at 100-370°C and annealed at 120-350°C (5 hours). Fig. 2 shows the pattern from the unformed steel (1, 2); the intensity spots fall up to 35% from the K_{α_1} and K_{α_2} lines. The spot size is indicated.

Card 1/2

X-ray Microbeam Studies of Ultrafine Grained Metals. I. 1/126-8-3-12/73

Fig. 2 shows a typical ultrafine grained metal structure of randomly distributed grains. It is concluded that the individual grains in fact consist of several plates of very small thickness. These plates, which are not the same size, because they are themselves nonuniform, have a randomly distributed thickness parameter. There are 7 figures in 7 references, 3 of which are Soviet, 4 English.

ASSOCIATION: Kharkovskiy polisskikh metallov Institut imeni
V. I. Lenin (Kharkov Polisskikh Metallov Institut imeni
V. I. Lenin)

SUBMITTED: July 20, 1956 (initially); November 27, 1957 (after
revision)

1. Steel--Microstructure
2. X-ray diffraction analysis--Applications
3. X-ray diffraction analysis--Equipment
4. Crystals--Lattices

Card 2/2

AUTHOR: Fuks, M. Ya.
Gol'dshteyn, Ya.

TITLE: X-Ray Investigation of Deformed Steel by Means of
Micro-beams Part II (Kontsepnaya i eksperimental'naya issledovaniya
deformirovaniya stali s pomoshch'yu mikropechek. II)

PERIODICAL: Fizika Metalliv i Metallovedeniye, 1958, Vol 6,
Nr 4, pp 673-681 (USSR)

ABSTRACT: Use of narrow "micro-beams" of X-rays is very promising
from the point of view of studying plastically deformed
metals, since they enable obtaining important new
information on the deformation of individual crystallites.
In this paper some of the results are described which
were obtained in investigations by means of this method
of carbon steels which were subjected to tension at
various speeds. The specimens made of the carbon steel
25 were subjected to normalisation annealing at
860-870°C and tempering at 620 to 630°C with subsequent
slow cooling. From these standard specimens were
prepared for long duration tensile tests. According to
earlier work of the authors (Ref 1), the average linear

Card 1/6

X-Ray Investigation of Deformed Steel by Means of Micro-beams.
Part II.

dimension of the crystallites in the non-deformed state equals 2.0×10^{-2} nm. Specimens were investigated after fracture in long or short duration tensile tests; the test conditions and the results are entered in a table, p. 61. The method of X-ray analysis was the same as that described in earlier work (Ref. 1). The X-ray exposures were taken from sections of the specimens with residual elongations of 6.15 and 40%. The surface of the specimens was first etched to a depth of 0.5 mm for the purpose of eliminating the layer which becomes work hardened during machining. The diffraction patterns were obtained by means of irradiation with the direction of the primary beam perpendicular to the direction of the deformation of the specimen and perpendicular to the specimen axis. The interference pattern from the plane (220) was investigated. The diameter of the irradiated section amounted to 0.7 mm or 120 μ in the case of a convergence of the primary beam of

Card 2/6

07/126-6-4-15/34

X-Ray Investigation of Deformed Steel by Means of Micro-Beams.
Part II.

1.9×10^{-3} to 25×10^{-3} rad. The exposure time was 30 to 40 hours. A common feature of all the X-ray diffraction pictures of the deformed specimens, obtained by the micro-beam method, is that instead of single sharply defined spots, which are characteristic for non-deformed specimens, separate arcs were observed, Fig.1. These arcs consist of groups of more or less pronounced individual spots or continuous black lines. The regularity of distribution of the spots in the arc (slight displacement of the spots in the radial direction), which was observed in a number of cases, indicates that adjacent spots in the arcs correspond to adjacent fragments or at least fragments which are very near to each other. Therefore, the magnitude of angular deorientation calculated from the angle between adjacent spots in the arc characterises the degree of deorientation of the fragments in the crystallite. Results are given for the following conditions of experiment: fracture by tensile stresses applied for 137 hours at 450°C ; fracture by tensile stresses at 450°C applied for 15.5 hours; fracture by tensile stresses at 450°C applied for a

Card 3/6

80V/126-6-4-15/34

X-Ray Investigation of Deformed Steel by Means of Micro-Beams.
Part II.

duration of 3 mins; fracture of a specimen after deformation in the cold state; investigation of the influence of the texture; long duration stressing of the steel 35KtNM (at 500°C). The conclusions of the authors can be summarised thus:

1. It is shown that it is possible to apply the method of micro-beams for the purpose of studying the plastic deformation of steels.
2. Long duration stretching of "Steel 25" at 450°C is accompanied by refining of the fragments in the crystallites and their deorientation. The degree of deorientation of the fragments increases with increasing speed and degree of deformation. The magnitude of the angle of deorientation of the fragments in the investigated cases fluctuate between 5 and 40 mins and the magnitude of the total area of deorientation in the individual crystallite fluctuates within the limits of a few degrees. A fine structure was detected of some fragments formed during deformation.

Card 4/6

100-10-10-10

X-Ray Investigation of Deformed Steel by Means of Micro-Beams.
Part II.

3. In the case of deformation in the cold state of "Steel 25", the breaking away and decementation of the fragments is considerably more intensive and distortions which occur in the fragments are larger than they are for an equal deformation speed at 450°C.
4. Deformation in the cold state and subsequent annealing at 450°C does not transform the fine structure of the steel into the same state as short duration deformation at 450°C, i.e. the effects of deformation and heating on the structure of the metal are not additive.
5. Fragments in crystallites of deformed "Steel 25" are not equivalent to mosaic blocks and are considerably larger than the latter. However, this does not exclude at all the existence of a mosaic structure of the fragments themselves.
6. Long duration stretching of steel 55HNM, the composition of which is more complex, is accompanied by a greater breaking up of the crystallites than long duration stretching of "Steel 25" at 450°C.
7. The obtained results lead to the assumption that an

Card 5/6

107/1204-4-15/34

X-Ray Investigation of Deformed Steel by Means of Micro-Beams.
Part II.

increase in the deorientation between fragments brings about an increase in the work hardening of the metal.
8. The sliding mechanism of fragment formation plays a fundamental role in the long duration stretching of carbon steel 25 as well as of the steel 35KhNM, under the conditions pertaining in the experiments described in the paper. There are 6 figures, 1 table and 3 references of which 3 are Soviet and 2 English.

ASSOCIATION: Khar'kovskiy Politehnicheskii Institut (Khar'kov Polytechnical Institute)

SUBMITTED: 20th June 1960

Card 6/6

PHASE I BOOK EXPLANATION NOV/57

Metallurgy, 1957, No. 3 (Physical Metallurgy/Collection of Articles, No. 3), Moscow, 1957, 340 p. 3,400 copies printed.

Ed.: O. I. Kopylov, Candidate of Technical Sciences; Literary and Tech. Ed.: S. I. Burdakov.

NOTE: This collection of articles is intended for scientific personnel at research and educational institutions and industrial plants and also for advanced students.

CONTENTS: The articles report the results of investigations of 1) the effect of various factors on the susceptibility of constructional and heat-resistant steels and titanium alloys to brittle failure at various temperatures under various conditions of loading (long-time, short-time, cyclic, non-cyclic) 2) alloying, strengthening and heat treatment of alloys as related to their mechanical properties, and 3) corrosion resistance of alloys and steels and heat-resistant steels. The articles are accompanied by numerous Soviet and non-Soviet references. No personalities are mentioned.

Zav'yalov, A. S., Doctor of Technical Sciences, Professor. Names of Steel-Embrittlement Processes During Heating and the Effect of Alloying Elements on Them

Topolov, Ye. D., Candidate of Technical Sciences; S. S. Topolov, Engineer; and Ye. A. Mironov, Engineer. Effect of Nickel and Copper on Thermal Brittleness of Chromium-Nickel-Titanium Constructional Steel

Miron, L. S., Doctor of Technical Sciences; and T. E. Mironov, Engineer. Mechanism of Hydrogen Embrittlement in Steel

Gilmanov, L. A., Doctor of Technical Sciences, Professor; B. S. Kolyatin, Engineer; V. P. Tschernov, Candidate of Chemical Sciences; and V. I. Derzhavina, Engineer. Change in Mechanical Properties of Certain Steels Under the Action of Hydrogen at High Temperatures and Pressure

Miron, L. S., and Ye. D. Mironov, Engineer. Investigation of the Mechanism of Hydrogen Embrittlement of Titanium and Its Alloys

Shchepin, S. I., Candidate of Technical Sciences. Role of Intermetallic Structures in the Heat Treatment of Nickel-Alloy Constructional Steel

Goldmanov, L. Ye., Engineer. Stability of Structures and Properties of Superalloys

Kuchinskii, A. L., Candidate of Technical Sciences. Microscopic and Macroscopic Cracks in Cast-Inducted Steel

Chernomir, V. I., Engineer. Sensitivity of Titanium and Its Aluminum Alloys to Brittle Failure Under Compression Loading

Glebov, B. A., Candidate of Technical Sciences. Investigation of the Relationship Between Size of Dislocation and Development of the First Failure Cracks in Testing Steel for Mechanical Properties

Belikov, R. G., Doctor of Technical Sciences, Professor. Some Characteristics on the Strength of Metals as Related to Their Alloying Elements

Burdakov, S. S., Candidate of Technical Sciences. Investigation of the Initial Portions of Stress-Strain Diagrams and Mechanism of Strains for Substructural Steel

13(7)

SOV/48-23-5-12/31

AUTHORS: Fuks, M. Ya., Gol'dshteyn, L. Ya.

TITLE: Investigation by the Aid of an X-Ray Microbeam of Steel Deformed With Varied Velocity at Increased Temperature (Issledovaniye pri pomoshchi rentgenovskikh mikropuchkov stali, deformirovannoy s razlichnoy skorost'yu pri povyshennoy temperature)

PERIODICAL: Izvestiya Akademii nauk SSSR. Seriya fizicheskaya, 1959, Vol 23, Nr 5, pp 629-634 (USSR)

ABSTRACT: By way of an introduction the authors refer to similar investigations carried out by B. A. Movchan, Ye. V. Kolontsova and B. M. Rovinskiy. St.25 was the steel type investigated, the samples were standardized and subsequently, as shown in table 1, they were deformed within different time intervals, with temperature amounting to 450°C. Investigations were carried out with a fine-focus X-ray tube (system according to B. Ya. Pines). Investigations are then extended to the non-deformed state of the samples, in which connection the special inhomogeneities of the lattice period and the disorientation of the structural parts were specially considered. Two microphotograms are shown in this connection, that were taken in the tangential and radial direction of the samples. Investigation results of the deformed state are summarized in table 1.

Card 1/2

907/48-23-5-10, 71
Investigation by the Aid of an X-Ray Microbeam of Steel Deformed With
Varied Velocity at Increased Temperature

Concerning the deformation stages of 6%, 15% and 40% the disorientations of the structural parts determined on the strength of the microphotographs are shown for the various deformation times. There is a strong dependence observable in disorientation on velocity and degree of deformation, namely, disorientation increases with velocity and degree of deformation. The results obtained from the same investigations on the steel type 35KhNM are then compared; the dimensions of the crystallites of this steel are lower by half as compared with those of St.25. It follows from the results thus obtained that in the range of deformation velocity investigated the macroscopic deformation of steel at 450°C is in relation with a displacement mechanism of the structural parts. There are 5 figures, 1 table, and 5 references, 4 of which are Soviet.

Card 2/2

KOGAN, L.S.; GOL'DSHTEYN, L.Ya.

Some properties of fused cements. TSement 26 no.2:7-13
Mr-Ap '60. (MIRA 13:6)

(Cement)

S/137/62/000/003/138/191
A052/A101

AUTHORS: Semenov, M. Ye., Voskoboinikov, D. B., Gol'dshteyn, L. Ya.

TITLE: The effect of aluminum on the strength of bimetallic compound of zinc alloy with steel

PERIODICAL: Referativnyy zhurnal, Metallurgiya, no. 3, 1962, 60, abstract 3I384 ("Vestn. Vses. n.-i. in-ta s.-d. transp.", no. 6, 1961, 42-43)

TEXT: The effect of Al on the formation of Fe-Zn-phases in the metal used for zinc-plating was investigated, as well as its effect on the formation of the transition zone and on mechanical properties of a bimetallic compound. An addition of 0.2% Al raises the resistance to shearing stress of the bimetallic compound to 27 kg/mm² compared with 23.3 kg/mm² without an Al addition. The presence of 2% Cu reduces the resistance to shearing stress to 14.8 kg/mm². An increase of Al content to 9% has just a slight effect on the resistance to shearing stress. It is recommended to increase the Al content in LAM 9-1,5 (TsAM 9-1,5) Zn-alloy to 0.5 - 0.7% to prevent the formation of FeZn₄ in the bath and to facilitate the cleaning of the bath from the ferrous components (in this case FeAl₃ is formed which comes to the surface).
[Abstracter's note: Complete translation]

E. Volin

Card 1/1

S/137/52/000/005/083/150
AC06/A101

AUTHORS: Lyubarskiy, I. M., Voskoboinikov, D. B., Gol'dshcheyn, I. Ya.

TITLE: Changes in the fine structure and hardness of low-carbon rimming steel depending on the heat treatment conditions and the duration of mechanical aging

PERIODICAL: Referativnyy zhurnal, Metallurgiya, no. 5, 1962, 24, abstract 5113C ("Tr. Donetsk. politekh. in-ta", 1961, 56, 1 1-158)

TEXT: Changes in the fine structure were studied by the X-ray method and by measuring the hardness of low-carbon grade 2Kh (2kp) and 3Kh (3kp) steel during mechanical aging; the steel had previously been subjected to various kinds of heat treatment. The investigation was carried out on specimens of 10 x 10 x 10 mm size, cut out of specimens for toughness tests. The impact specimens were subjected to a certain type of heat treatment (8 variants), tensile deformation by 10%, and aging at 250°C for 1 or 50 (50) hours. Radiographs were taken by the method of reverse exposure on a plane container in a KPOC -1 (KROC-1) camera, in emission of Co-anode of an X-ray, type ECBJ (BSVL), tube. The width of line (310) K α was investigated. Radiographs taken by the Deb
Card 1/2

Changes in the fine structure and hardness ...

3/137/62/000/005/083/156
A036/A101

Debye method, at angles of 35 and 90°, are also presented. It was established that during deformation, the width of line (310) K_{α} increases sharply for all investigated types of preliminary heat treatment. Maximum relative increase in the line width takes place in high-tempered steel, least increase in quenched steel. During the aging process changes occur in the fine steel structure, caused by high-temperature tempering phenomena and mechanical aging proper. It is pointed out that the kinetics and nature of fine-structural changes in steel during mechanical aging depend substantially on the type of preliminary heat treatment; quenched steel is the most resistant to aging. The method of cooling after tempering does not affect the nature of changes in the fine structure of the steel during mechanical aging. Increased duration of mechanical aging over one hour is accompanied by some reduction of hardness in such specimens which showed higher hardness values after heat treatment. There are 5 references.

Z. S.

[Abstracter's note: Complete translation]

Card 2/2

S/805/62/000/003/017/018

AUTHORS: Busha, N. A., Lyubarskiy, I. M., Voskoboynikov, D. B.,
Gol'dshteyn, L. Ya.

TITLE: "Bulging" of lead babbitt.

SOURCE: Akademiya nauk SSSR. Institut metallurgii. Issledovaniye splavov
tsvetnykh metallov. no.3. 1962, 194-203.

TEXT: The paper describes a recently discovered problem peculiar to the low-tin (appx. 2% Sn) babbitt BK2 (BK2), not observed on any high-tin babbitt, namely, the "bulging" of the babbitt layers in separate points of a bearing. The investigation was conducted by the All-Union Scientific Research Institute of Railroad Transportation and the Diesel-Locomotive Factory imeni Malyshev. Most frequently the babbitt layer exhibits large bulges, up to 20-mm diam, with separation of the babbitt layer from the backing. Fissures visible to the naked eye appear on the surface of the bulges. Some bearing inserts exhibit small pimples of up to 2 mm diam, which are not accompanied by insert / backing separation or the appearance of surface fissures. The bulging was observed on inserts stored in both dry and moist conditions, with a protective lubricant layer and without any lubricant. While the bulges may appear anywhere, the large bulges form preferably on the

Card 1/3

"Bulging" of lead babbitt.

S/806/62/000/003/017/018

darker oxidized portions of the insert surface. Bulges have not been manifest in inserts installed on operating engines, neither has any great incidence of insert failures by fissuration or crumbling of the babbitt layer been reported. Statistical analysis shows that bulging correlates with an increase of ingot babbitt and decrease of scrap babbitt in the smelting charge, also with the change from air cooling to water cooling, which is intended to produce a finer-grain structure. In fact, the composition of BK2 underwent a sharp change in 1957, and is no longer the alloy originally tested in 1949-51. The Ca content has thus changed from 0.06-0.16% to 0.36, the Na from 0.15-0.31 to 0.45%; concurrently the H_B has changed from 15-20 to 25-32. It was found experimentally (near-full-page table) that all inserts suffering from large or small bulges had an excessive amount of Na, namely, in excess of the saturation amount at room T (0.4%). All nondefective stored specimens had Na contents less than 0.4%. The Ca content was not critical. The Mg content in all specimens was below standard (0.04-0.09%). The microstructure of all bulged inserts was the fine-crystalline structure of a rapidly-cooled babbitt. Conclusions: The low-Na alloy used prior to 1957 aged less intensely, the high-Na alloy produced since 1957 ages more intensely, with segregation of a Ca-rich secondary phase (Pb_3Ca , Pb_3Na , and $PbMg_2$) in a finely-dispersed state.

Microstructural analysis on aged and over-aged specimens (detail explanation and

Card 2/3

"Bulging" of lead babbitt.

S/806/62/000/003/017/018

photos shown) revealed sizable distortions along the babbitt-grain boundaries in the presence of a large amount of Na. The dissolved gases trapped in water-cooled cast specimens diffuse along the boundaries and add to the residual stresses, until bulging occurs. The increased oxidation of bulging inserts is an indication that corrosion processes are at work also. All other conditions being equal, bulging occurs preferably in inserts that exhibit casting defects (cavities, etc.) and inadequate insert-to-backing adhesion. Specifications have been established for: (1) Content: 0.06-0.20% Ca, 0.15-0.30% Na, 0.03-0.09 Mg, 1.5-2.5% Sn, the remainder Pb; (2) hardness: H_V 23 after 72 hrs following casting; (3) gas content: Measures have been taken (unspecified) to reduce the freezing rate of the babbitt and reduce the amount of dissolved gases. There are 5 figures, 2 tables, and 7 Russian-language Soviet references.

ASSOCIATION: None given.

Card 3/3

GOL'DSHTEYN, L.Ya.; SLIVA, Ya.

Analysis of the mineralogical composition of fused portland-
cement clinkers. Trudy Giprotsement no.24:26-35 '62.
(MIRA 16:4)

(Cement clinkers--Analysis)

GOL'DSHTEYN, L.Ya.

Some properties of fused cements. TSement 28 no.1:9-10 Ja-F
'62. (MIRA 16:5)

(Cement--Testing)

TRACHEV, V.V., inzh.; GOL'DSHTEIN, L.Ya., inzh.

Technical consultation. TSement 28 no.4:24 JI-Ag '62. (MIRA 15:7)

1. Gosudarstvennyy institut proyektirovaniya predpriyatiy i po
nauchno-issledovatel'skim rabotam tsementnoy promyshlennosti.
(Cement industries)

KOGAN, L. S.; GOLDSHTEYN, L. Ya.

Characteristics of preparing mixes during the production of fuel
clinkers on the mineral part of Baltic Sea region oil shale.
Trudy Giprotsement no. 26:29-44 '63. (MIRA 17:5)

GOLDSHTEYN, L. Ya.; SAVINA, V. N.; KOPILEVICH, V. S.; KORMSYEV, V. I.

Determining the viscosity of cement raw material mixtures in a
pyro-plastic state. Trudy Giprotsement no. 26:130-142 '63.
(MIRA 17:5)

COMPOSITION, L. Y., OF PORTLAND CEMENT

Fused portland cement with reduced value of α coefficient
of saturation. Truly (improvement no. 11) 1953-1954

HP-17-12

GOL'DSHEYN, G.Ya.; KOPILEVICH, V.S.

Characteristics of the fusability of portland cement raw material mixtures. Trudy Giprotsement no.27:37-55 '63.

(MIRA 17:12)

GOL'DSHTEYN, L. Ya.

Fusibility of raw cement mixes. TSement 29 no.2:6-8 Mr..Ap '63.
(MIRA 16:4)

1. Gosudarstvennyy institut po proyektirovaniyu predpriyatiy
i nauchno-issledovatel'skim rabotam tsementnoy promyshlennosti.

(Cement—Testing)

THE

... ..
... ..

GOL'DSHTEYN, L. Ye.

Quantitative distribution of fungi-microphytes in the southwestern
Kyzylkum. Uzb. biol. zhur. 8 no.4:38-41 '64. (MIRA 18:7)

1. Institut botaniki AN UzSSR.

GOL'DSHTEYN, L.Ya.; OKOROKOV, S.D.

Possibility of considerably increasing the content of free CaO and MgO of Portland cements during their manufacture by the fusion method. Dokl. AN SSSR 159 no.2:420-422 N '64.

(MIRA 17:12)

1. Predstavleno akademikom P.A. Rebinderom.

L 20239-65 EWT(m)/EWA(d)/T/EWP(t)/EWP(b) MJW/JD
ACCESSION NR: AP5000937 S/0129/64/000/012/0039/0041

AUTHOR: Balter, M. A.; Dukaravich, I. S.; Gol'dshtern, L. Ya.

TITLE: Phase composition of boronized steel layer G

SOURCE: Metallovedeniye i termicheskaya obrabotka metallov, no. 12, 1964, 39-41, and insert facing p. 25

TOPIC TAGS: boronizing, steel boronizing, boronized layer thickness, carbon steel boronizing, alloy steel boronizing, boronized layer property

ABSTRACT: The phase composition, depth, and the hardness of the boronized layer and transition zone in several steels were determined in order to compare the suitability of the steels for boronizing and to establish the effect of alloying elements on the properties of the boronized layer. It was found that the chemical composition of carbon and low-alloy steels has no essential effect on the rate of boron diffusion. Higher carbon content decreases the diffusion rate only with prolonged (over 3 hr) boronizing. Chromium at contents of

Card 1/32

L 20239-65

ACCESSION NR: AP5000937

0.9—1.5% has no significant effect on the depth of the boronized zone. However, titanium or combinations of silicon, molybdenum, aluminum, or chromium, tungsten, and manganese reduce the rate of boron diffusion. In high alloy steels, such as 3Kh2B8, 1Kh12, 2Kh11, G13L, and Kh18N9T, the maximum thickness of the boronized layer only amounted to 0.03—0.08 mm, and the layer peeled off easily. The structure of the boronized layer in all investigated steels was similar: 70—90 vol. % needle-shaped borides and the remainder, δ -phase with boride inclusions. The microhardness (Hv) was 1300—1400 for Fe_2B , 420—1170 for a mixture of α -phase and borides, and 600—980 for the carbide phase. The structure of the transition zone differed from the structure of the core, and the micro-hardness of the transition zone was 50—100 kg/mm² higher than that of the core owing to carbon diffusion toward the center. This diffusion of carbon changed the chemical compositions and properties of the transition zone and made the rate of boron diffusion almost independent of carbon content. Orig. art. has: 4 figures.

ASSOCIATION: none

Card 2/3

"APPROVED FOR RELEASE: 09/24/2001

CIA-RDP86-00513R000515710013-8

APPROVED FOR RELEASE: 09/24/2001

CIA-RDP86-00513R000515710013-8"

(N) L 12089-66 EWT(m)/EWP(w)/EWA(d)/T/EWP(t)/EWP(r)/EWP(b)/EWA(c) MJW/ED
 ACC NR: AP6000608 SOURCE CODE: UR/0129/65/000/012/0030/0033
 AUTHOR: Parshin, A. M.; Gol'dshteyn, L. Ya.; Pechnikov, I. I.; Leonova, N. I. 42
 40
 B
 ORG: none
 TITLE: Hardening of Kh18N22V2 austenitic chromium nickel steel after aging at 600-750°C
 SOURCE: Metallovedeniye i termicheskaya obrabotka metallov, no. 12, 1965, 30-33
 TOPIC TAGS: austenitic steel, metal hardening, chromium steel, nickel steel, phase analysis/ Kh18N22V2T2 austenitic chromium-nickel steel
 ABSTRACT: Austenitic Cr-Ni steels alloyed with 1.3-3% Ti are widely used; their high mechanical properties are achieved by short (10-20 hr) aging at 700-750°C following austenitization. Yet the mechanism of this hardening, as well as the microstructural transformations occurring in the steels considered, has not yet been adequately investigated. Hence, the authors investigated specimens of industrially manufactured Kh18N22V2T2 steel subjected to austenitization at 1200°C (for 1 hr) with subsequent water quenching followed by isothermal aging at 500-950°C for up to 5000 hr. These specimens were subjected to tensile and impact-bending tests at room temperature and their microstructure was examined by means of optical and electron microscopes as well as selective oxidation. Findings: impact strength decreases at temperatures at which tensile strength increases; resistance to impact loading decreases with in-
 Cord 1/3 UDC: 621.785.74:669.14.018.89

* Error: Journal states X18H2282T2 2

L 12089-66

ACC NR: AP6000608

2

creasing aging time; at 1200°C (1 hr, water quenching) the microstructure of the steel consists of austenite and primary carbonitrides of the Ti(C, N) type and there are no excess phases on grain boundaries and twins. Hardening of this steel is accomplished only after aging at 600-750°C. Depending on the time and temperature of aging, the following intermetallide phases may appear in Kh18N22V2T2 steel: a) phases β -Ni₃Ti with face-centered cubic lattice; b) phases α -Ni₃Ti with hexagonal tightly packed lattice; c) phases Fe₂Ti with hexagonal tightly packed lattice; d) σ -phases of the Fe(Cr, W) type with β -uranium type lattice. A comparison of the changes occurring in the mechanical properties of Kh18N22V2T2 steel at room temperature with the changes in microstructure owing to aging indicates that the most intense hardening of the material, accompanied by a decrease in impact strength (and plasticity) occurs during the period when no changes as yet are detected in the steel's microstructure. Hence, hardening during this stage of aging is not associated with the segregation of a discrete β -Ni₃Ti phase and, instead, is caused by preparatory processes within the austenite grains (redistribution of Ti) preceding the segregation. The hardening of steel at 600-750°C may be attributed to elastic distortions of the austenite lattice in the pre-segregation zones of the β -Ni₃Ti phase and to the steel's inability for stress relaxation under these conditions. Softening with increasing time of aging (e.g. at 750°C) is conditioned by the stress relaxation occurring on the formation, segregation and coagulation of the β -Ni₃Ti phase. Thus, hardening is caused by preparatory processes within the grains of the solid solution, preceding the segregation of this phase, whereas softening, on the other hand, is caused by the segregation of

Card 2/3

L 12089-66

ACC NR: AP6000608

the intermetallide. These findings also refute the contention of Sorokin et al. (Zavodskaya laboratoriya, 1959, no. 6) and Blok et al. (Zavodskaya laboratoriya, 1957, no. 8) that hardening is attributable to the formation of the intermetallide phase β -Ni₃Ti with face-centered cubic lattice. Orig. art. has: 5 figures

SUB CODE: 11, 13. SUBM DATE: none/ ORIG REF: 003/ OTH REF: 000

Card 3/3

PARSHIN, A.M.; GOL'DSHTEYN, L.Ya.; PECHNIKOV, I.I.; IL'KOVA, N.I.

Hardening of Kh12N22B2T2 steel following aging at 600-750° C.
Metalloved. i term. obr. met. no. 12:30-33 D 124.

(MIRA 15:12)

ACC NR: AR6027505

SOURCE CODE: UR/0137/00/000/000/1020/1020

AUTHOR: Parshin, A. M.; Gol'dshteyn, L. Ya.; Pechnikov, I. I.; Leonova, N. I.

TITLE: Strengthening of Kh18N22V2T2 steel after aging at 600-750°C

SOURCE: Ref. zh. Metallurgiya, Abs. 41132

REF SOURCE: Metallovedeniye i term. obrabotka metallov, no. 12, 1965, 30-33

TOPIC TAGS: high strength steel, austenite steel, metal aging, stress relaxation / Kh18N22V2T2 steel

TRANSLATION: Sheets of Kh18N22V2T2 steel were aged isothermally at 500-950°C for periods up to 5000 hr, after austenitizing at 1200°C with subsequent water quenching. The steel samples were tested in tension and impact bending. Microstructures were analyzed by light and electron microscopes as well as by x-rays. Strengthening occurred only after aging at 600-700°C. Thus, after aging for 1 hr at 650°C, σ_b was increased to 16 kg/mm². In the course of subsequent aging for periods of 500 hr, σ_b increased to 21 kg/mm². After aging for 5000 hr at 750°C, intensive softening occurred in the steel. The strengthening of the steel at 600-750°C was explained by elastic distortions of the austenitic lattice in the α -Ni₃Ti pre-precipitation zones and by the resistance of the steel to stress relaxation under these conditions. Softening during prolonged aging

UDC: 669.15'26'24'27'295.017.3:621.785.78

Card 1/2

ACC NR: AR6027505

was caused by stress relaxation during the formation and separation of the α -Ni₃Ti phase, as well as by its coagulation. I. Tulupova.

SUB CODE: 11,13

Card 2/2

RODKINA, Raisa Abramovna; MIL'CHENKO, I.T., prof., doktor med. nauk,
red.; KOZHEVNIKOVA, V.A., red.; GOL'DSHTEYN, L.Ye., red.;
SPIEIDONOV, N.F., tekhn. red.

[Cancer of the cervix uteri and its stages] Rak sheinoi matki i
stadii. Kuibyshev, Kuibyshevskii med.in-t, 1960. 205 p.
(MIRA 15:4)

(UTERUS—CANCER)

GETSELEV, Vladimir Borisovich; TERTYSHNIK, Grigoriy Afanas'yevich;
GOL'DSHTEYN, L.Ye., redaktor; SHCHERBAKOV, A.I., tekhnicheskii
redaktor

[At the thick of life] V gushche zhizni. [Kuibyshev] Kuibyshevskoe
kn-vo, 1955. 57 p. (MIRA 9:8)
(Collective farms)

MOLOCHNIKOV, L.N.; GOL'DSHTEYN, L.Ye., red.; SPIRIDONOV, N.F., tekhn. red.

[Operation and repair of electric dredging equipment] Eksploatatsiia
i remont elektricheskikh zemsnariadov. Pod red. M.B. Miasodova.
[Kuibyshev] Kuibyshevskoe knizhnoe izd-vo, 1955. 89 p. (MIRA 11:8)
(Dredging machinery--Maintenance and repair)

NAUMENKO, German Vladimirovich; GOL'DSHTEYN, L.Ye., redaktor; SHCHERBAKOV,
A.I., tekhnicheskii redaktor

[Bright temper of steel parts] Svetlyi otpusk stal'nykh detalei.
[Kuibyshev] Kuibyshevskoe knizhnoe izd-vo, 1956. 11 p. (MIRA 10:9)
(Steel--Heat treatment)

BYLINKIN, Petr Petrovich; GOL'DSHTEYN, L.Ye., redaktor; ENTROPOL'SKAYA,
N.Ye., redaktor; SHCHERBAKOV, A.I., tekhnicheskij redaktor

[Collective creativity; how we increase labor productivity]
Kollektivnoe tvorchestvo; kak my povyshаем proizvoditel'nost' turda.
[Kuibyshev] Kuibyshevskoe knizhnoe izd-vo, 1956. 16 p. (MLRA 10:9)

1. Starshiy master zavoda KATEK (for Bylinkin)
(Machinery industry)

PETROV, Ivan Prokhorovich; TRAKHTENBERG, B.F., kandidat tekhnicheskikh nauk, redaktor; GOL'DSHTEYN, L.Ye., redaktor; SHCHERBAKOV, A.I., tekhnicheskii redaktor

[Production of high-strength magnesium cast iron] Proizvodstvo vysokoprochnogo magniivogo chuguna; iz opyta Syzranskogo gidroturbinnogo zavoda. Pod red. B.F.Trakhtenberga. [Kuibyshev] Kuibyshevskoe knizhnoe izd-vo, 1956. 42 p. (MLRA 10:9)
(Cast iron--Metallurgy)

GOL'DSHTEYN, L.Ye., red.

[City of Kuybyshev] Gorod Kuibyshev. [Kuibyshev] Kuibyshevskoe
knizhnoe izd-vo, 1957. 260 p. (MIRA 11:10)
(Kuybyshev--Description)

MIT'KEVICH, Georgiy Petrovich; MALEYEVA, Lyudmila Nikolayevna; PUTOKHIN,
N.I., doktor khim.nauk, nauchnyy red.; GOL'DSHTEYN, L.Ye., red.;
YASHEN'KINA, Ye.A., tekhn.red.

[Plastics, a new building material] Plastmassy - novyi stroi-
tel'nyi material. Kuibyshev, Kuibyshevskoe knizhnoe izd-vo, 1958.
26 p. (MIRA 13:12)

(Plastics)

IVANOV, Nikolay Vasil'yevich; FOMINYKH, L.I., kand.ekon.nauk,dots.,
red.; GOL'DSHTEYN, L.Ye., red.; YASHEN'KINA, Ye.A., tekhn.
red.

[Concentration of production and the specialization of enter-
prises of local state industry]Kontsentratsiia proizvodstva i
spetsializatsiia predpriiatií mestnoi gosudarstvennoi pro-
myshlennosti. Kuibyshev, Kuibyshevskii planovoi in-t, 1961. 55 p.
(MIRA 15:8)

(Kuibyshev Province---Industrial management)

SOBOLEV, I.M.; SIMANKOV, G.M., otv. red.; KOVALEV, O.I., red.; KOGAN,
I.B., red.; LOVYAGIN, N.V., red.; NAZAROVA, N.V., red.;
GOL'DSHTEYN, L.Ye., red.; DURASOVA, V.M., tekhn.red.

[Guidebook to the city of Kuybyshev] Putevoditel' po gorodu
Kuibyshevu. Kuibyshev, Kuibyshevskoe knizhnoe izd-vo, 1962.
319 p. (MIRA 16:9)

(Kuybyshev--Guidebooks)